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(54) **INPUT CLAMPING STRUCTURE FOR SOUND QUALITY IMPROVEMENT IN CAR-RADIO CLASS-AB POWER AMPLIFIER DESIGN**

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This patent is subject to a terminal disclaimer.

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(30) **Foreign Application Priority Data**

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**H03F 3/21** (2006.01)  
**H03F 3/26** (2006.01)

**H03F 3/187** (2006.01)  
**H03F 3/45** (2006.01)  
**H03F 3/68** (2006.01)

(52) **U.S. Cl.**  
CPC ..... **H03F 3/211** (2013.01); **H03F 3/187** (2013.01); **H03F 3/26** (2013.01); **H03F 3/4508** (2013.01); **H03F 3/45475** (2013.01); **H03F 3/68** (2013.01); **H03F 2200/03** (2013.01); **H03F 2203/21131** (2013.01); **H03F 2203/45102** (2013.01); **H03F 2203/45154** (2013.01); **H03F 2203/45244** (2013.01); **H03F 2203/45528** (2013.01); **H03F 2203/45552** (2013.01)

(58) **Field of Classification Search**  
None  
See application file for complete search history.

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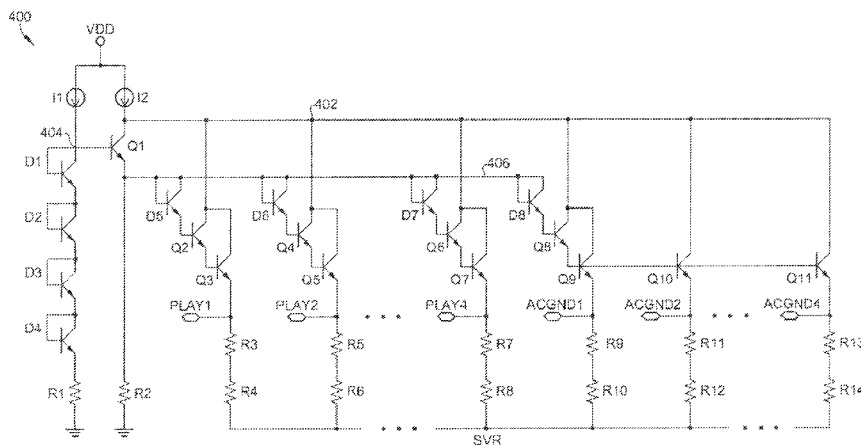
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(57) **ABSTRACT**

A clamping circuit for a class AB amplifier includes a reference voltage circuit, four NPN Darlington transistors having inputs coupled to the reference voltage circuit, and outputs for providing four clamped voltages and a split NPN Darlington transistor having an input coupled to the reference voltage circuit, and four separate outputs for providing four AC ground voltages.

**24 Claims, 7 Drawing Sheets**



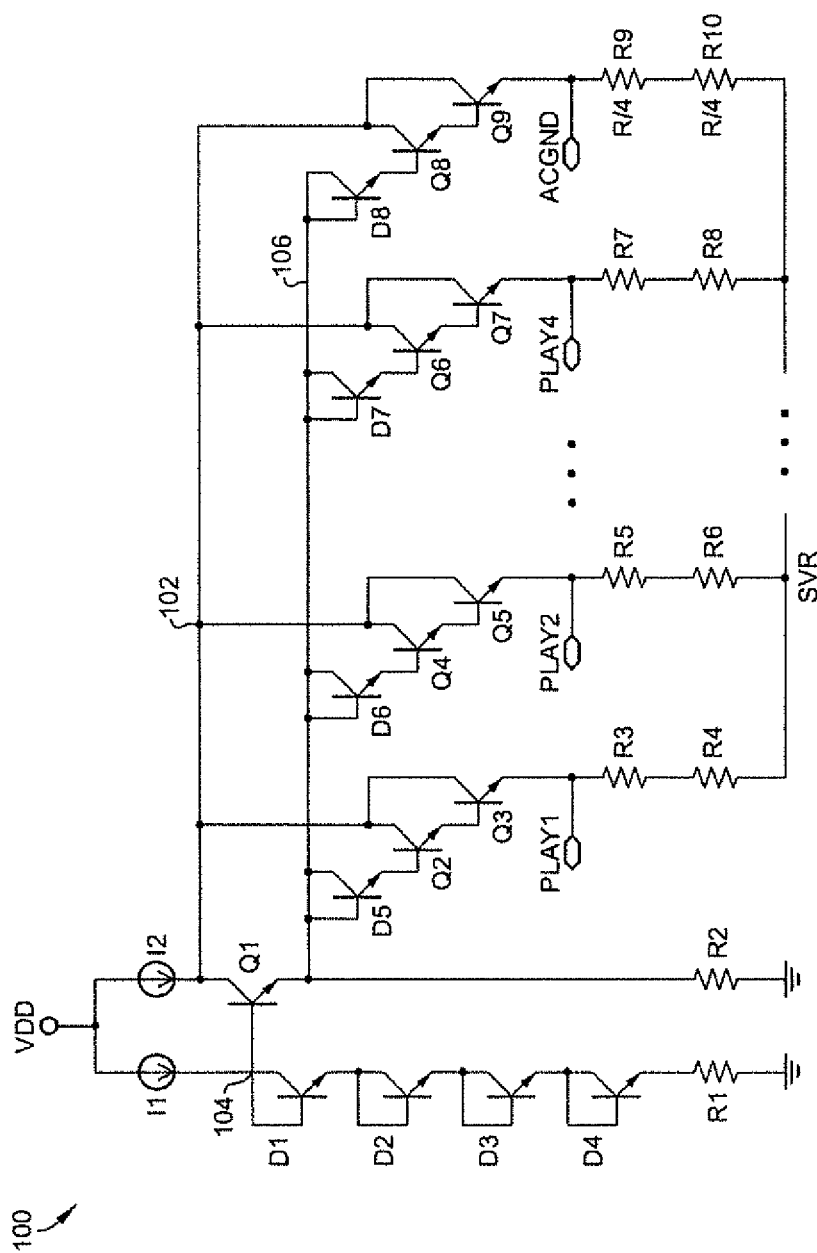


Fig. 1  
(PRIOR ART)

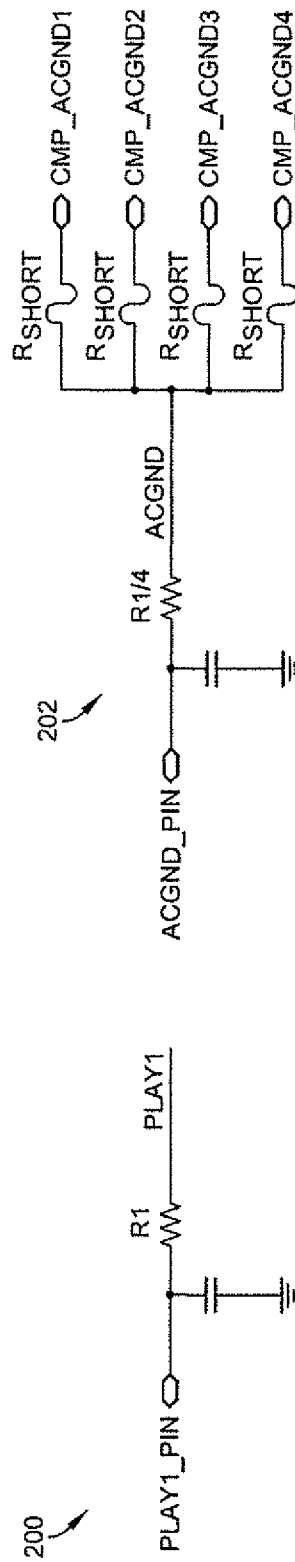


Fig. 2  
(PRIOR ART)

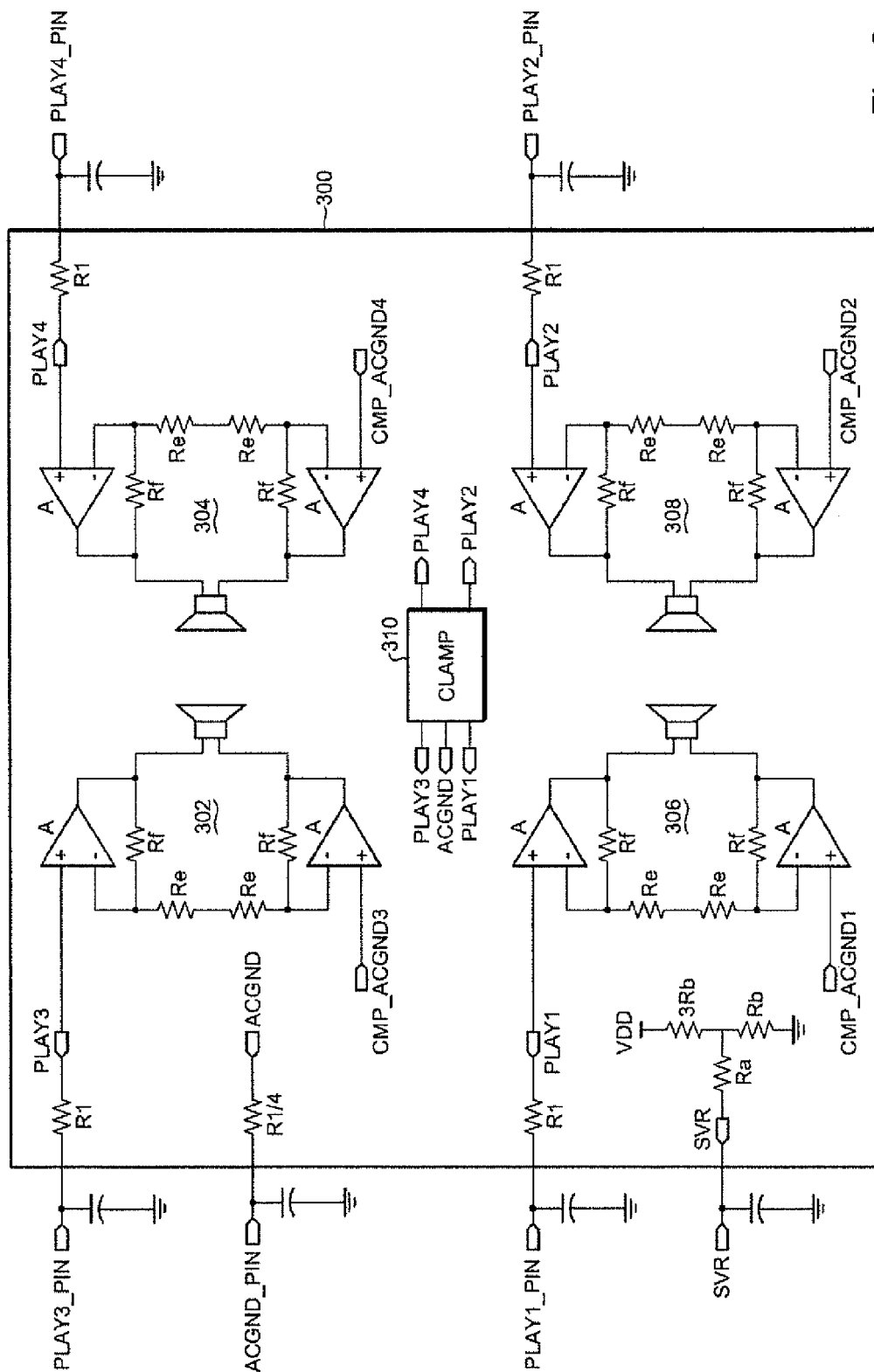


Fig. 3  
(PRIOR ART)

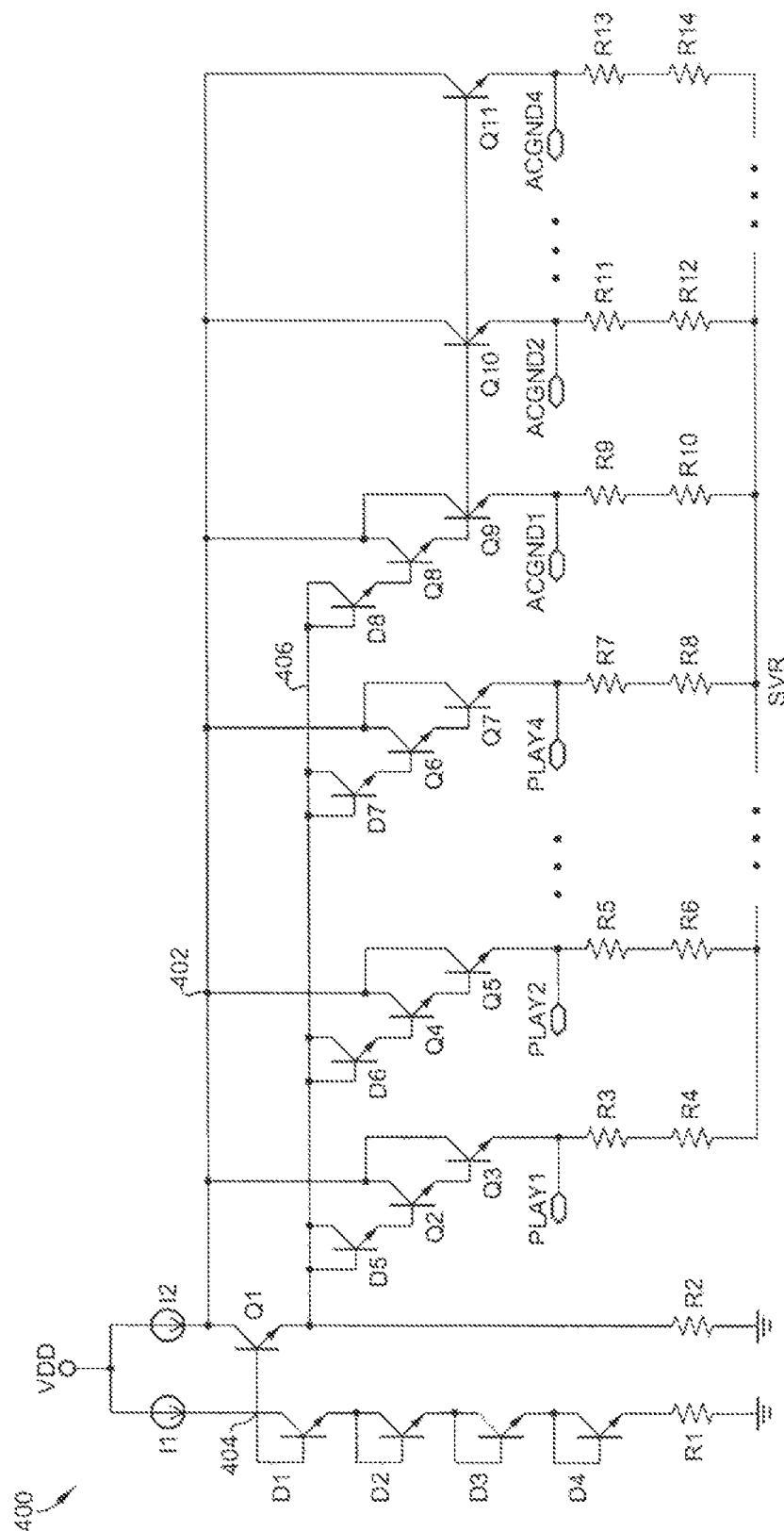


Fig. 4

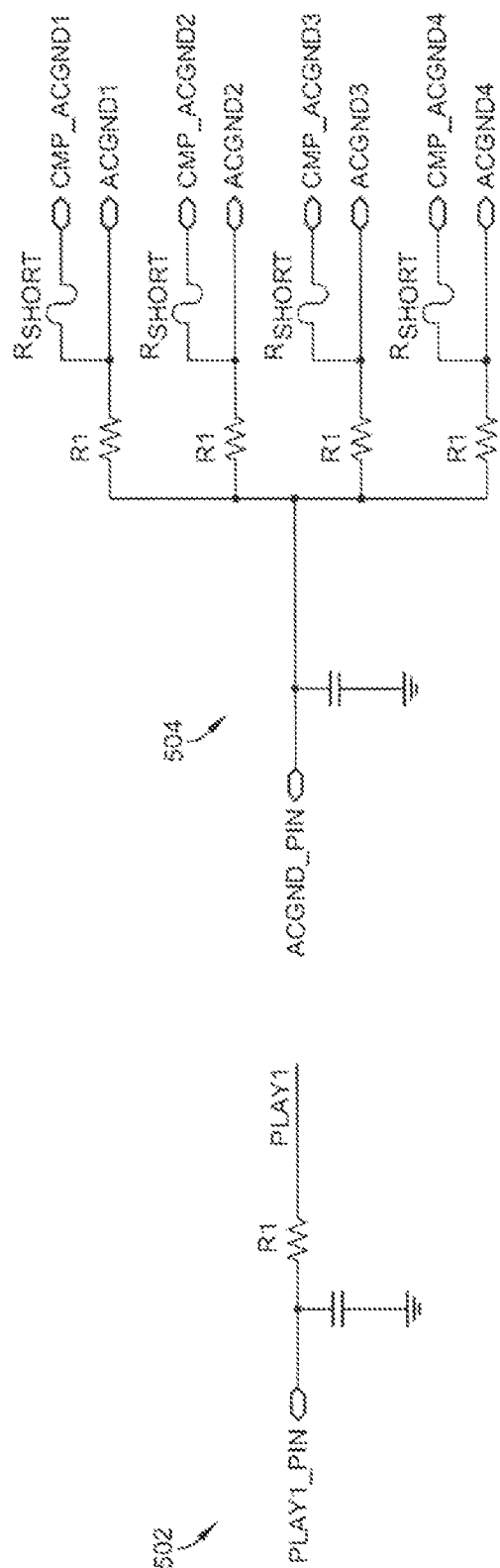


Fig. 5

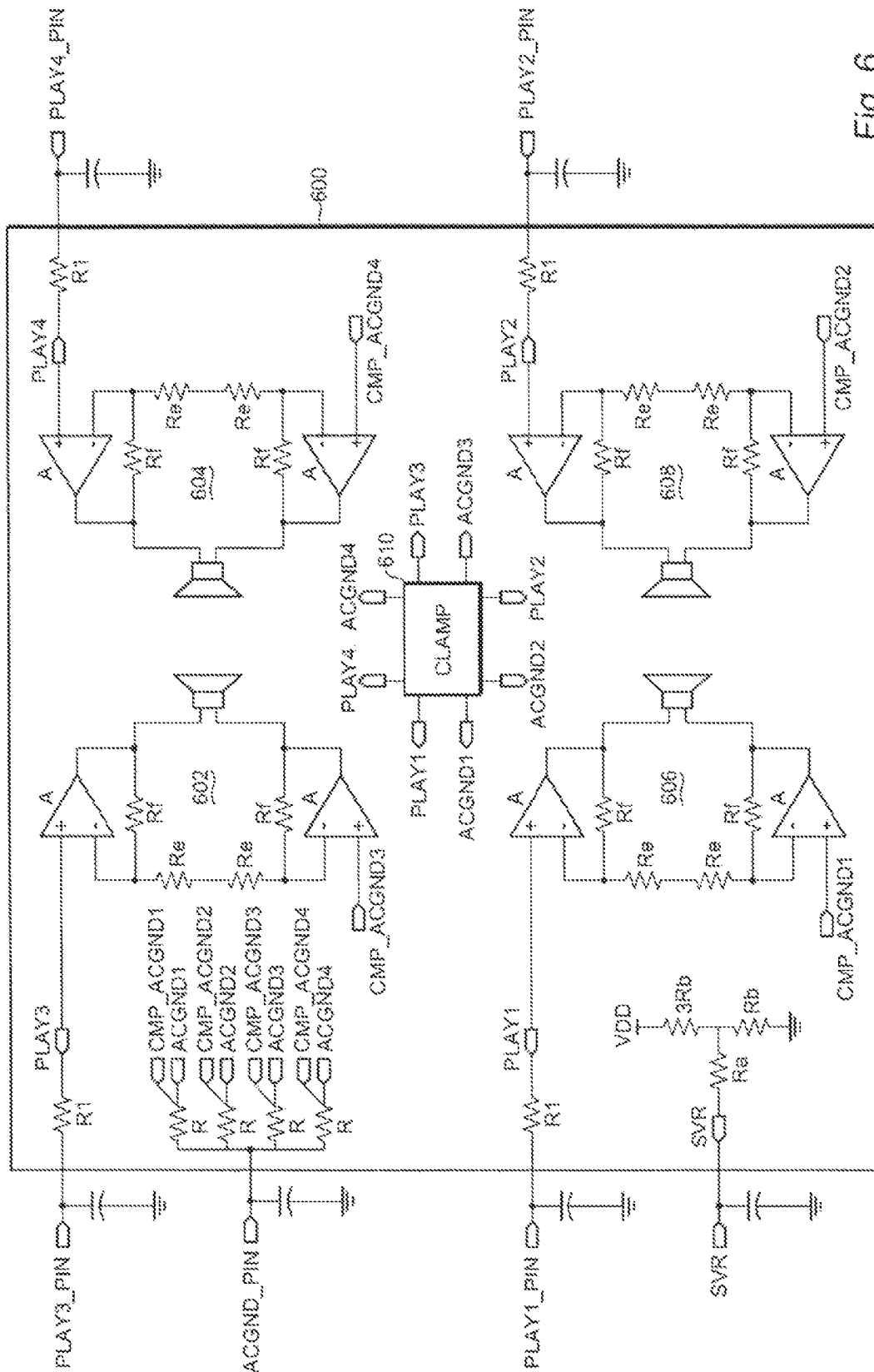


Fig. 6

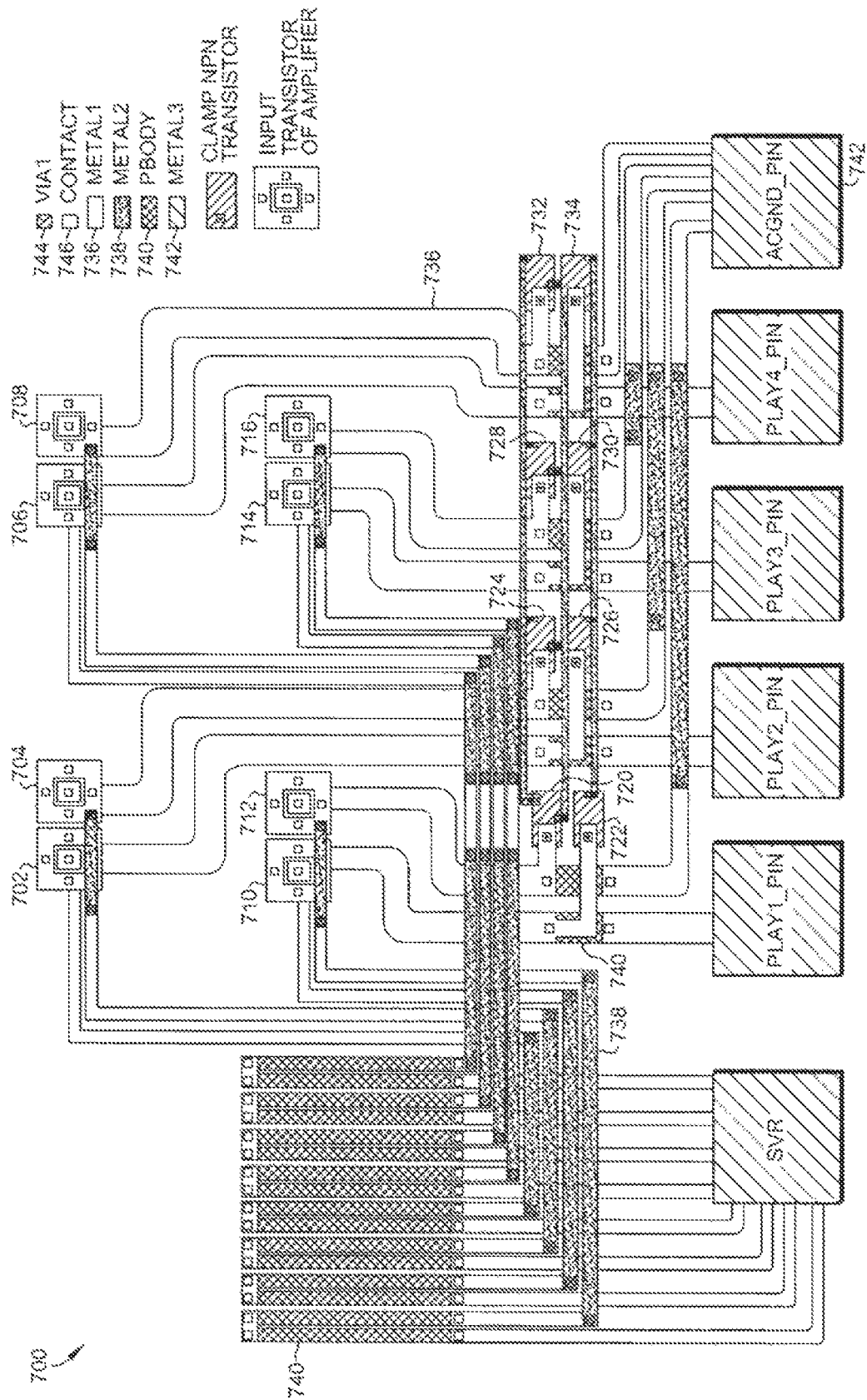


Fig. 7



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# INPUT CLAMPING STRUCTURE FOR SOUND QUALITY IMPROVEMENT IN CAR-RADIO CLASS-AB POWER AMPLIFIER DESIGN

## RELATED APPLICATION

This application is a translation of and claims the priority benefit of Chinese patent application number 201110461474.2, filed on Dec. 30, 2011, entitled Input Clamping Structure For Sound Quality Improvement in Car-Radio Class-Ab Power Amplifier Design, which is hereby incorporated by reference to the maximum extent allowable by law.

## FIELD OF THE INVENTION

The present invention relates to class AB power amplifiers, and more particularly, to an input clamping circuit for improving sound quality of the amplifier.

## BACKGROUND OF THE INVENTION

A typical input clamping structure **100** for a class AB power amplifier is shown in FIG. 1. Circuit **100** includes a reference voltage generator including a first leg comprising a first bias current **I1** (typically between 70 and 100 microamps) coupled to node **104**, serially coupled diodes **D1**, **D2**, **D3** and **D4**, and resistor **R1** (typically about 3K ohms). A second leg of the reference voltage generator comprises a second bias current **I2** (typically between 70 and 100 microamps), a transistor **Q1** having a drain for receiving the **I2** bias current at node **102**, a base coupled to node **104**, and an emitter coupled to resistor **R2** (typically about 30K ohms). The voltage at node **104** is about 3.3 volts. The two bias currents are also coupled to VDD, which is typically set at about 144 volts for a power amplifier. The clamping circuit also includes four NPN Darlington transistors **Q2/Q3**, **Q4/Q5**, . . . **Q6/Q7** for generating clamped input voltages **PLAY1**, **PLAY2**, . . . **PLAY4**. The **PLAY1** node is coupled through resistors **R3** and **R4** to the SVR node. The values of resistors **R3** through **R10** is about 25K ohms. The SVR node stands for "Supply Voltage Rejection" and is an internal reference node set to about VDD/4. The serially coupled resistors are shown for better matching and routing in layout design of an integrated circuit. Similarly, the **PLAY2** node is coupled through resistors **R3** and **R6** to the SVR node, and the **PLAY4** node is coupled through resistors **R7** and **R8** to the SVR node. The ACGND node is coupled through resistors **R9** and **R10** to the SVR node. NOTE that the value of resistors **R9** and **R10** is one fourth the value of the **PLAY** node resistors. ACGND is the common node corresponding to nodes **PLAY1** to **PLAY 4**, as will be seen and described in further detail below, and so these resistors must be four resistors in a parallel connection.

In FIG. 2 **PLAYx** and **CMP\_ACGNDx** are the direct inputs to the amplifier input stage, in the layout of the integrated circuit the star-point the metal traces to the destination must be coming from the same point although each of the metal traces are at the same potential) is from ACGND in FIG. 2, and  $R_{short}$  is the routing metal resistance. Resistor **R1** is about 600 ohms and **R1/4** is about 600 ohms, divided by four. Note that the resistors shown in FIG. 2 are different than those shown in FIG. 1. In FIG. 2, there are four ACGND nodes that correspond to four input nodes. The four ACGND nodes (**CMP\_ACGND1**, **CMP\_ACGND2**, **CMP\_ACGND3**, and **CMP\_ACGND4**) are coupled to the same point (ACGND)

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and the four inputs (**PLAY1**, **PLAY2**, **PLAY3**, and **PLAY4**) are independent. The capacitors shown in FIG. 2 represent discrete capacitors that are used in conjunction with the class AB amplifier integrated circuit.

The integrated circuit class AB amplifier **300** is shown in FIG. 3, including amplifier pair **302**, amplifier pair **304**, amplifier pair **306**, amplifier pair **308**, and clamp circuitry **310**. The input and ground connections are all as previously described. In FIG. 3, the **Rf** resistors are typically 8K ohms, and the **Re** resistors are typically 400 ohms. The class AB amplifier **300** is shown in a typical audio application for driving loudspeakers. While the amplifier **300** shown in FIG. 3 achieves a good level of performance, it is limited by the unbalanced ground connection. What is desired is a class AB amplifier that has the highest level of audio performance and least amount of distortion with a completely separate and balanced ground connection.

## SUMMARY OF THE INVENTION

According to the present invention, a novel input clamping structure for a car-radio class-AB power amplifier has ACGND node that is separated into four discrete branches. Correlative pad connection optimization and layout constraints are adopted to improve sound quality.

According to the present invention, a clamping circuit for an AB amplifier comprises a reference voltage circuit, a plurality of NPN Darlington transistors having a plurality of inputs coupled to the reference voltage circuit, and a plurality of outputs for providing a plurality of clamped voltages, and a split NPN Darlington transistor having an input coupled to the reference voltage circuit, and a plurality of outputs for providing a plurality of AC ground voltages. The reference voltage circuit comprises a first leg comprising a first bias current, a plurality of serially coupled diodes, and a resistor, and a second leg comprising a second bias current, a transistor, and a resistor. The clamping circuit further comprises a plurality of input diodes interposed between the reference voltage circuit and the plurality of Darlington transistors, and a plurality of emitter resistors coupled to the plurality of Darlington transistors. The clamping circuit also further comprises an input diode interposed between the reference voltage circuit and the split Darlington transistor, and an emitter resistor coupled to the split Darlington transistor.

According to the present invention, an AB amplifier circuit includes a plurality of AB amplifiers each having a play input and a ground input and a clamping circuit comprising a plurality of play outputs respectively coupled to each play input and plurality of separate and balanced ground outputs respectively coupled to each ground input.

According to the present invention, a corresponding clamping method for an AB amplifier according to the present invention includes providing first, second, third, and fourth input clamp signals to the AB amplifier, and providing first, second, third, and fourth corresponding balanced and separate AC ground signals to the AB amplifier.

## BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic diagram of a typical input biasing circuit for a class AB power amplifier according to the prior art;

FIG. 2 is a schematic diagram of further details regarding the inputs to the class AB power amplifier;

FIG. 3 is a schematic diagram of a class AB amplifier and damping circuitry according to the prior art;

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FIG. 4 is a schematic diagram of an input biasing circuit for a class AB power amplifier according to the present invention;

FIG. 5 is a schematic diagram of further details regarding the separated inputs to the four amplifier bridges in the class AB amplifier according to the present invention;

FIG. 6 is a schematic diagram of a class AB amplifier and clamping circuitry according to the present invention; and

FIG. 7 is a plan view of a layout of the class AB amplifier and clamping circuitry according to the present invention.

#### DETAILED DESCRIPTION

According to the present invention, a clamp circuit and a class AB circuit incorporating the clamp circuit is shown in FIGS. 4-6. The ACGND node is separated into four separate and balanced branches. Since current injected to ACGNDx is the same as PLAYx, the resistor between SVR and ACGNDx is also changed to the same as that between SVR and PLAYx, so PLAYx and ACGNDx are completely balanced and matching is much better in the corresponding layout.

Referring now to FIG. 4, a clamping circuit 400 includes a reference voltage circuit as before, and a plurality of Darlington transistors as before. Previous nodes 102, 104, and 106 are relabeled 402, 404, and 406 in FIG. 4. Note that a split NPN Darlington transistor Q8, Q9, Q10, . . . , Q11 is shown having an input coupled to the reference voltage circuit at node 406, and a plurality of outputs for providing a plurality of AC ground voltages ACGND1, ACGND2, . . . , and ACGND4. An input diode D8 is interposed between the reference voltage circuit and the split Darlington transistor. Clamping circuit 400 comprises a plurality of emitter resistors R9/R10, R11/R12, R13/R14 coupled to the split Darlington transistor. The value of each of the resistors shown in FIG. 4 is 25K ohms.

FIG. 5 shows circuitry 502 and 504 that provides corresponding connections to circuit pads. Circuit 502 shows the signal input connections, and circuit 504 shows the balanced and separate ground connections. The PLAYx\_PIN, ACGND\_PIN and SVR nodes are external pad connections, and the rest of the circuit nodes are internal. The circuit elements of FIG. 5 are shown in the context of the AB amplifier circuit in FIG. 6. The star-point is from the pad of ACGND in layout. The star-point from SVR to the resistors inside inputs the biasing circuit starts also directly from SVR pad. The CMP\_ACGNDx nodes go to the ground input of the AB amplifiers, and the ACGNDx nodes are coupled to the clamp circuit. The capacitors shown in FIG. 5 are discrete capacitors, external to the integrated circuit including the class AB amplifiers and the clamp circuit. A resistor R1 is associated with each signal input PLAYx\_PIN to PLAYx node and each ground connection ACGND\_PIN to ACGNDx node.

Referring now to FIG. 6, a class AB amplifier circuit including a clamp circuit 600 is shown. Circuit 600 in class AB amplifiers 602, 604 606 and 608, as well as clamp circuit 610. Each class AB amplifier includes four internal resistors as shown. The values of the Rf and Re resistors are the same as identified with the prior art amplifier shown in FIG. 3. Each PLAYx\_PIN includes an external capacitor, a series resistor R1, and a PLAYx node coupled to a positive input of a first operational amplifier of the corresponding class AB amplifier. The ACGND\_PIN includes an external capacitor, four series resistors R, which in turn is coupled to the CMP\_ACGNDx and ACGNDx nodes. The CMP\_ACGNDx nodes are coupled to a positive input of a second operational amplifier of the corresponding class AB amplifier. The ACGNDx nodes are provided by the clamp circuit 610. The SVR pin includes an external capacitor and is coupled to the internal SVR node. The SVR node is coupled to resistor Ra,

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which is in turn coupled to the center tap of resistors Rb and 3Rb. Resistors Rb and 3Rb are coupled between VDD and ground.

In the present invention, a clamp circuit having separated and well balanced ground connections is used to improve sound quality. Layout optimization is also of great importance. The layout design should obey the rule strictly to match and balance every inputs of the amplifier and the general layout guidelines should always be implemented.

Referring now to FIG. 7, a layout 700 for the integrated circuit according to the present invention is shown. The SVR, PLAY1\_PIN, PLAY2\_PIN, PLAY3\_PIN, PLAY4\_PIN, and ACGND\_PIN pins are shown. Input transistors 702 and 704 correspond to the input differential pair receiving the PLAY2 and CMP\_ACGND2 voltages, input transistors 706 and 708 correspond to the input differential pair receiving the PLAY4 and CMP\_ACGND4 voltages, input transistors 710 and 712 correspond to the input differential pair receiving the PLAY1 and CMP\_ACGND1 voltages, and input transistors 714 and 716 correspond to the input differential pair receiving the PLAY3 and CMP\_ACGND3 voltages. Layout 700 also includes clamping transistors 720 and 722 that correspond to transistor Q3 and Q7, clamping transistors 724 and 726 that correspond to transistors Q6 and Q9, clamping transistors 728 and 730 that correspond to transistors Q7 and Q10, and clamping transistors 732 and 734 that correspond to the transistors used to clamp the PLAY3 and ACGND3 voltages (not shown). Also shown in FIG. 7 are vias 744 that couple a first metal level 736 to a second metal level 738, and contacts 746 that couple resistors to the first metal level 736. Pbody resistors shown in FIG. 7 correspond to resistors R3 through R12 (left side of the figure) and resistor R1 (center of figure). All of the pins in FIG. 7 are provided by a third level of metal 742.

It is important to note that all of the signal inputs and the ground connections shown in the layout of FIG. 7 are separate and balanced. Other variations of the layout 700 shown in FIG. 7 are of course possible while providing the balanced signal and ground connections according to the present invention. Due to the balanced layout and design of the present invention the class AB amplifier circuit will provide a much improved sound quality.

In summary a damping method for an AB amplifier includes providing first, second, third, and fourth input clamp signals to the AB amplifier, and providing first, second, third, and fourth corresponding separate and balanced AC ground signals to the AB amplifier.

It will be apparent to those skilled in the art therefore, that various modifications and variations can be made to the invention without departing from the spirit or scope of the invention. Thus, it is intended that the present invention covers the modifications and variations of this invention provided they come within the scope of the appended claims.

We claim:

1. An AB amplifier circuit comprising:
  - a plurality of AB amplifiers;
  - a plurality of Darlington transistors having a plurality of inputs coupled to a reference voltage, and a plurality of outputs configured to provide a plurality of clamped voltages to the plurality of AB amplifiers; and
  - a split Darlington transistor comprising
    - a first transistor and a second transistor coupled together in a Darlington configuration, and
    - at least one third transistor coupled to the second transistor,
    - the first transistor, second transistor and at least one third transistor having inputs coupled to the reference voltage,

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the second transistor and at least one third transistor having a plurality of outputs configured to provide a plurality of AC ground voltages to the plurality of AB amplifiers.

2. The AB amplifier circuit of claim 1 wherein the plurality of AB amplifiers are arranged in pairs with each pair comprising:

a clamp input coupled to a respective output from the plurality of Darlington transistors; and  
an AC ground input coupled to a respective output from the split Darlington transistor.

3. The AB amplifier circuit of claim 1 further comprising a reference voltage circuit configured to provide the reference voltage and comprising a first leg comprising a first bias current source, a plurality of serially coupled diodes coupled to the first bias current source, and a resistor coupled in series with the serially coupled diodes.

4. The AB amplifier circuit of claim 3 wherein the reference voltage circuit comprises a second leg comprising a second bias current source, a transistor coupled to the second bias current source, and a resistor coupled in series with the transistor.

5. The AB amplifier circuit of claim 1 wherein the plurality of Darlington transistors comprises a plurality of NPN Darlington transistors.

6. The AB amplifier circuit of claim 1 further comprising a plurality of input diodes coupled between the reference voltage and respective ones of the plurality of Darlington transistors.

7. The AB amplifier circuit of claim 1 further comprising a plurality of emitter resistors coupled to respective ones of the plurality of Darlington transistors.

8. The AB amplifier circuit of claim 1 wherein the split Darlington transistor comprises an NPN split Darlington transistor.

9. The AB amplifier circuit of claim 1 further comprising an input diode coupled between the reference voltage and the split Darlington transistor.

10. The AB amplifier circuit of claim 1 further comprising a plurality of emitter resistors coupled to the split Darlington transistor.

11. The AB amplifier circuit of claim 1 wherein the at least one third transistor comprises a plurality of third transistors.

12. An electronic device comprising:

a plurality of AB amplifiers;  
a plurality of NPN Darlington transistors having a plurality of inputs coupled to a reference voltage, and a plurality of outputs configured to provide a plurality of clamped voltages to the plurality of AB amplifiers; and

a split NPN Darlington transistor comprising  
a first transistor and a second transistor coupled together in a Darlington configuration, and  
at least one third transistor coupled to the second transistor,

the first transistor, second transistor and at least one third transistor having inputs coupled to the reference voltage,

the second transistor and at least one third transistor having a plurality of outputs configured to provide a plurality of AC ground voltages to the plurality of AB amplifiers.

13. The electronic device of claim 12 wherein the plurality of AB amplifiers are arranged in pairs with each pair comprising:

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a clamp input coupled to a respective output from the plurality of NPN Darlington transistors; and  
an AC ground input coupled to a respective output from the split NPN Darlington transistor.

14. The electronic device of claim 12 wherein further comprising a reference voltage circuit configured to provide the reference voltage and comprising a first leg comprising a first bias current source, a plurality of serially coupled diodes coupled to the first bias current source, and a resistor coupled in series with the serially coupled diodes.

15. The electronic device of claim 14 wherein the reference voltage circuit comprises a second leg comprising a second bias current source, a transistor coupled to the second bias current source, and a resistor coupled in series with the transistor.

16. The electronic device of claim 12 further comprising a plurality of input diodes coupled between the reference voltage and respective ones of the plurality of Darlington transistors.

17. The electronic device of claim 12 further comprising a plurality of emitter resistors coupled to respective ones of the plurality of Darlington transistors.

18. The electronic device of claim 12 further comprising an input diode coupled between the reference voltage and the split NPN Darlington transistor.

19. The electronic device of claim 12 further comprising a plurality of emitter resistors coupled to the NPN split Darlington transistor.

20. The electronic device of claim 12 wherein the at least one third transistor comprises a plurality of third transistors.

21. A method of operating a plurality of AB amplifiers arranged in pairs with each pair comprising a clamp input and an AC ground input, the method comprising:

operating a plurality of Darlington transistors having a plurality of inputs coupled to a reference voltage, and a plurality of outputs providing a plurality of clamped voltages to the clamp inputs of the plurality of AB amplifiers; and

operating a split Darlington transistor comprising  
a first transistor and a second transistor coupled together in a Darlington configuration, and  
at least one third transistor coupled to the second transistor,

the first transistor, second transistor and at least one third transistor having inputs coupled to the reference voltage,

the second transistor and at least one third transistor having a plurality of outputs providing a plurality of AC ground voltages to the AC ground inputs of the plurality of AB amplifiers.

22. The method of claim 21 further comprising operating a voltage reference circuit to provide the reference voltage; and wherein the reference voltage circuit comprises a first leg comprising a first bias current source, a plurality of serially coupled diodes coupled to the first bias current source, and a resistor coupled in series with the serially coupled diodes.

23. The method of claim 22 wherein the reference voltage circuit comprises a second leg comprising a second bias current source, a transistor coupled to the second bias current source, and a resistor coupled in series with the transistor.

24. The method of claim 21 wherein the plurality of Darlington transistors comprises a plurality of NPN Darlington transistors; and the split Darlington transistor comprises an NPN split Darlington transistor.

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